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1.6-6 CONT.

$$A_b = 259.8 \text{ mm}^2 - 113.1 \text{ mm}^2 = 146.7 \text{ mm}^2$$

$$\sigma_b = \frac{P}{A_b} = \frac{9.0 \text{ kN}}{146.7 \text{ mm}^2} = 61.3 \text{ MPa} \leftarrow$$

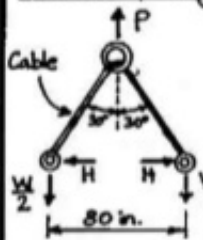
(b) Shear stress in head of bolt

$$A_s = \text{shear area} = \pi dt$$

$$\tau_{\text{AVE}} = \frac{P}{A_s} = \frac{P}{\pi dt} = \frac{9.0 \text{ kN}}{\pi (12 \text{ mm})(6 \text{ mm})} = 39.8 \text{ MPa} \leftarrow$$

1.6-7 Steel plate hoisted by a sling

Free-body diagram of sling



d = diameter of clevis pins = 0.70 in.
 W = weight of steel plate

Weight of steel plate
 $W = (\text{weight density})(\text{volume}) = \gamma V$; $\gamma = 490 \text{ lb/ft}^3$
 $V = (100 \text{ in.})(50 \text{ in.})(4 \text{ in.}) = 20,000 \text{ in.}^3$

$$W = (490 \text{ lb/ft}^3) \left(\frac{1}{1728} \frac{\text{ft}^3}{\text{in.}^3} \right) (20,000 \text{ in.}^3) = 5671 \text{ lb}$$

Tensile force T in cable

$$\sum F_{\text{VERT}} = 0 \uparrow + \downarrow -$$

$$T \cos 30^\circ - \frac{W}{2} = 0$$

$$T = \frac{W}{2 \cos 30^\circ} = \frac{5671 \text{ lb}}{2 \cos 30^\circ} = 3274 \text{ lb}$$

Shear stress in the pins (double shear)

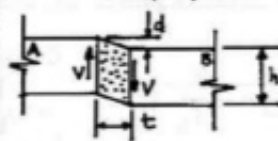
$$\tau_{\text{AVE}} = \frac{T}{2A_{\text{PIN}}} = \frac{3274 \text{ lb}}{2 \left(\frac{\pi}{4} \right) (0.70 \text{ in.})^2} = 4250 \text{ psi} \leftarrow$$

Bearing stress between steel plate & pins

$$A_b = (\text{thickness of plate})(\text{diameter of pin}) = (4.0 \text{ in.})(0.70 \text{ in.}) = 2.80 \text{ in.}^2$$

$$\sigma_b = \frac{T}{A_b} = \frac{3274 \text{ lb}}{2.80 \text{ in.}^2} = 1170 \text{ psi} \leftarrow$$

1.6-8 Epoxy Joint between concrete slabs



$h = 100 \text{ mm}$
 $t = 12 \text{ mm}$
 $L = 1.0 \text{ m}$
 $d = 0.048 \text{ mm}$
 $G = 960 \text{ MPa}$

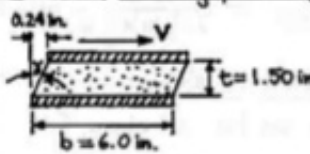
(a) Average shear strain

$$\gamma_{\text{AVE}} = \frac{d}{t} = 0.004 \leftarrow$$

(b) Shear forces V

Average shear stress: $\tau_{\text{AVE}} = G \gamma_{\text{AVE}} = 3.84 \text{ MPa}$
 $V = \tau_{\text{AVE}}(hL) = 384 \text{ kN} \leftarrow$

1.6-9 Bearing pad subjected to shear



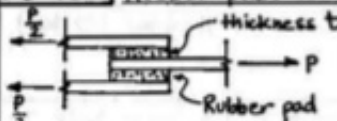
$V = 1200 \text{ lb}$
 Width of pad: $a = 5.0 \text{ in.}$
 Length of pad: $b = 6.0 \text{ in.}$

$$\tau_{\text{AVE}} = \frac{V}{ab} = \frac{1200 \text{ lb}}{(5.0 \text{ in.})(6.0 \text{ in.})} = 40 \text{ psi}$$

$$\gamma_{\text{AVE}} = \frac{0.24 \text{ in.}}{1.50 \text{ in.}} = 0.160$$

$$G = \frac{\tau}{\gamma} = \frac{40 \text{ psi}}{0.16} = 250 \text{ psi} \leftarrow$$

1.6-10 Rubber pads bonded to steel plates



Rubber pads: $t = 12 \text{ mm}$
 Length $L = 200 \text{ mm}$
 Width $b = 150 \text{ mm}$
 $G = 830 \text{ kPa}$
 $P = 15 \text{ kN}$

(a) Shear stress and strain in the rubber pads

$$\tau_{\text{AVE}} = \frac{P/2}{bL} = \frac{7.5 \text{ kN}}{(150 \text{ mm})(200 \text{ mm})} = 2.50 \text{ kPa}$$

$$\gamma_{\text{AVE}} = \frac{\tau_{\text{AVE}}}{G} = \frac{2.50 \text{ kPa}}{830 \text{ kPa}} = 0.301 \leftarrow$$

(b) Horizontal displacement

$$\delta = \gamma_{\text{AVE}} t = (0.301)(12 \text{ mm}) = 3.61 \text{ mm} \leftarrow$$



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